
## Department of Mechanical Engineering Michigan State University

Systems and Control Ph.D. Qualifying Examination

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Open Book Open Notes
All questions are weighted equally.

Prepared by

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1) A mechanical schematic for a print-head mechanism is shown in Figure 1-1. The particular variables of interest are the position and motion of the pin, x and y, respectively. Assume that the neutral position is at x = 0, with the pin centered subject to zero applied force F4. The force-deflection characteristics of the platen (at x=1) and the hard stop (at x=-1) are given by the {F2 vs. x} relations as if they were a single spring.

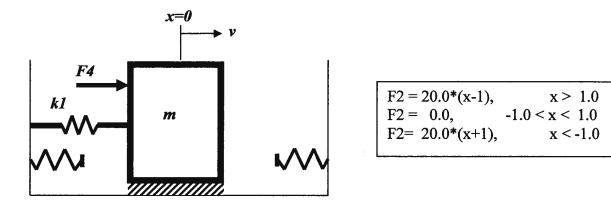


Figure 1-1. Print-head mechanism.

Parameters are given as follows (assume they are compatible SI units):

• m, mass of the pin

... m = 2.0

• k1, positioning spring

... k1 = 2.0

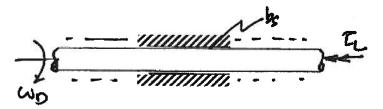
• F2 vs. x, effect of platen and stop ... (see above)

• b, friction effect when pin slides

... b = 0.2

- (a) Is the overall system linear or non-linear? Explain, please.
- (b) What constant force F4 is required to maintain the pin state as  $\{x=1, v=0\}$ ? Call this value Fcrit.
- (c) Choose F4=0.5\*Fcrit. The initial conditions are  $\{x=0, v=0\}$ . Predict the system response as precisely as possible.
- (d) Now set *F4= 0.98\*Fcrit*. Will your solution from part (b) still apply? Explain.
- (e) Now find F4 such that the steady-state is  $\{x=1.5, v=0\}$ . The initial conditions are  $\{x=1.4, v=0\}$ . v=0 \}. Predict the system response or else explain what difficulties you encounter that prevent that.

2) A long slender shaft rotates in a sleeve, as shown in Figure 2-1. The inputs to the shaft are the driving angular velocity  $\omega_D$  and load torque  $\tau_L$ .



PARAMETERS:

 $J_S = 1.0 \dots$  inertia of shaft  $K_S = 9.0 \dots$  shaft stiffness  $b_S = 0.1 \dots$  rotational friction

Figure 2-1. A rotating shaft.

## PART 1.

Assume a so-called "1-lump" model as shown in Figure 2-2.

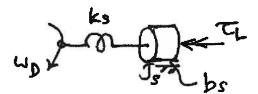


Figure 2-2. A "1-lump" model.

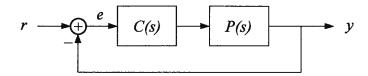
(a) If  $\omega_D = 10.0$  and  $\tau_L = 5.0$ , both constant, find the steady-state operating condition of the shaft. If there is a disturbance to the operating condition will there be oscillations in the shaft? Explain, please.

## PART 2.

Assume that we wish to use a "2-lump" model (i.e., a model with 2 masses and 2 springs) for improved accuracy. The inputs remain the same as in PART 1.

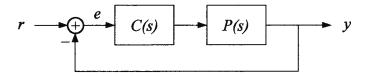
- (b) Sketch a "2-lump" model.
- (c) Find the eigenvalues, if you assume that b<sub>S</sub> is now zero. How do they relate to the eigenvalues of PART 1?

3) Consider the control system shown below with  $P(s) = \frac{(s+4)}{(s+\alpha)(s-2)}$ .



- (a) When C(s) = 1, sketch the locus of the closed-loop poles as  $\alpha$  varies in the interval  $0 \le \alpha < \infty$  and find the range of  $\alpha$  for which the closed-loop system is stable.
- (b) When C(s) = 1 and  $\alpha = 0$ , find the steady-state error due to a unit step input.
- (c) When  $\alpha=4$  and  $r(t)=\cos(t)u(t)$ , where u(t) is the unit step function, design a controller so that the output is asymptotically equal to the input. (Hint: Try a controller of the form  $C(s)=(k_1s^2+k_2s+k_3)/(s^2+\beta^2)$ , where  $k_1$ ,  $k_2$ ,  $k_3$  and  $\beta$  are the design parameters.)

4) Consider the control system shown below with  $P(s) = \frac{100(s+10)}{(s+1)(s+100)}$ .



- (a) Sketch the Bode plot of P(s)C(s) when C(s) = 1.
- (b) From the Bode plot, determine approximately the gain crossover frequency, phase crossover frequency, gain margin and phase margin. Is the closed-loop system stable?
- (c) Design a controller that satisfies the following design specifications: the steady-state error due to a step input is zero, the gain margin is at least 60 dB and the phase margin is at least 60°.